


<p>KLM Technology Group</p> <p>Practical Engineering Guidelines for Processing Plant Solutions</p>	 <p>Engineering Solutions</p> <p>www.klmtechgroup.com</p>	Page : 1 of 114
		Rev: 01
		Rev 01 – Jan 2016
<p>KLM Technology Group P. O. Box 281 Bandar Johor Bahru, 80000 Johor Bahru, Johor, West Malaysia</p>	<p>Kolmetz Handbook of Process Equipment Design</p> <p>ELECTRICAL POWER SUPPLY AND REGULATION</p> <p>(ENGINEERING DESIGN GUIDELINES)</p>	Co Author Riska Ristiyanti
		Editor / Author Karl Kolmetz

TABLE OF CONTENT

INTRODUCTION

Scope	8
General Consideration	9
DEFINITION	23
NOMENCLEATURE	25
Greek Letters	26

THEORY

I. TRANSFORMERS

a) Electromagnetic Transformers	28
b) The Ideal Transformers	32
c) Principles of Operation	38
d) Testing to Determine Transformer Parameters	39
e) Efficiency of a Transformer	41
f) Regulation of a Transformer	41

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 2 of 114
		Rev: 01
		Rev 01 – Jan 2016

g) Application 42

II. RECTIFIER AND FILTER CIRCUIT

a) Rectifier Circuit 45

b) Filter Circuit 53

III. SWITCHING POWER SUPPLIES

a) Linear Regulator Versus Switching Power Supplies 56

b) The Buck Regulator 58

c) The Boost Regulator 62

d) The Buck / Boost Regulator 66

e) The Fly back Regulator 70

f) The Half – Forward Regulator 74

g) The Push – Pull Regulator 77

h) The Full – Bridge Regulator 82

i) The Half – Bridge Regulator 86

IV. VOLTAGE REGULATION

a) Types of Voltage Regulation 91

b) Selecting a Voltage Regulator 92

c) Two Discrete Voltage Examples 93

d) IC Regulator Example 96

e) Voltage Regulator Packaging and Heat Sinking 102

REFERENCES

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 3 of 114
		Rev: 01
		Rev 01 – Jan 2016

LIST OF TABLE

Table 1	: Case to Heat Sink Thermal Resistance, θ_{cs}, for various Packages and Mounting Arrangements	105
Table 2	: Commercial Heat Sink Selection Guide	105

LIST OF FIGURE

Figure 1	: PWM Converter Methods : (a) direct duty cycle, (b) voltage feedforward control, (c) current mode control	11
Figure 2	: Non – Isolated Cuk Converter	12
Figure 3	: (a) Flyback converter. The clamp winding shown is optimal and is used to clamp the transistor voltage stress to $V_{in} + nV_o$ (b) Flyback converter waveforms without the clamp winding. The leakage inductance spikes vanish with the clamp winding.	13
Figure 4	: (a) Forward converter. The clamp winding shown is required for operation. (b) Forward converter waveforms.	14
Figure 5	: (a) Two – transistor single-ended fly back converter (b) Two – transistor single – ended forward converter	15
Figure 6	: Sepic Converter	15
Figure 7	: (a) Push – pull converter and (b) its opening waveforms	16
Figure 8	: Half – bridge converter. Coupling capacitor C_c, is used to avoid transformer saturation.	17
Figure 9	: Full – Bridge Converter	17
Figure 10	: (a) Zero – current resonant switch : (i) L – type and	

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 4 of 114
		Rev: 01
		Rev 01 – Jan 2016

	(ii) M – Type. (b) Half wave configuration using L – Type ZC resonant switch. (c) Full – wave configuration using L – Type ZC resonant switch	19
Figure 11	: (a) Zero – voltage resonant switches. (b) Half – wave Configuration Using ZV resonant switch shown in Figure 10 (a)(i). (c) Full – wave configuration using ZV resonant switch shown in Figure 10 (a)(i).	19
Figure 12	: (a) Implementation of ZCS QR buck converter using L – Type resonant switch. (b) Operating waveforms for half – wave mode. (c) Operating waveforms for full – wave mode.	20
Figure 13	: (a) Implementation of ZVS QR boost converter using resonant switch shown in Figure 11 (a) (i). (b) Operating waveforms for half–wave mode(c) Operating waveforms for full–wave mode.	21
Figure 14	: High-frequency resonant converter (half-bridge version) configurations suitable for operation above resonance. C_{n1} and C_{n2} are the snubber capacitors. (a) Series resonant converter. Leakage inductances of the HF transformer can be part of resonant inductance. (b)Parallel resonant converter. (c)Series-parallel (or LCC-type) resonant converter with capacitor C_t placed on the secondary side of the HF transformer.	22
Figure 15	: Flux paths in the core and windings of an iron cored transformer	27
Figure 16	: Linked Coils	29
Figure 17	: Dotted schematic symbol for a transformer	32
Figure 18	: Equivalent Circuit	33
Figure 19	: Low – frequency Equivalent Circuit	35

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 5 of 114
		Rev: 01
		Rev 01 – Jan 2016

Figure 20	: Midband Equivalent Circuit	36
Figure 21	: High – Frequency Model	37
Figure 22	: Ultra – High – Frequency Model	38
Figure 23	: Connection for Open – Circuit Test	39
Figure 24	: Short – Circuit Test Setup	40
Figure 25	: (a) Equivalent for 1:1, (b) Equivalent for step-up ($n > 1.0$), (c) equivalent for step down ($n < 1.0$)	44
Figure 26	: Pulse Terminology	45
Figure 27	: Half – Wave Rectifier : (a) Circuit Diagram, Input and Output Waveforms	46
Figure 28	: Full wave rectifier : (a) Schematic diagram, (b) Input and Output Waveforms	48
Figure 29	: Bridge rectifier : (a) Circuit Schematic, (b) Input and Output voltage waveforms	49
Figure 30	: Voltage doubler circuit : (a) diagram, (b) voltage across diode D_1	50
Figure 31	: A precision rectifier : (a) Circuit diagram, (b) an improved Version of the precision half-wave rectifier	51
Figure 32	: Precision full wave rectifier with a diode placed in the feedback loop	52
Figure 33	: A Precision bridge rectifier	53
Figure 34	: Half-wave and RC filter circuit : (a) schematic diagram, (b) input and output waveforms	53
Figure 35	: Filter Circuits : (a) full wave rectifier with L-section filter, (b) multiple L-section filter	55
Figure 36	: The Buck Regulator Topology	58

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 6 of 114
		Rev: 01
		Rev 01 – Jan 2016

Figure 37	: DC Wafeforms for a buck regulator	59
Figure 38	: AC Waveforms for a buck regulator	60
Figure 39	: The boost regulator topology	63
Figure 40	: DC waveform for a boost regulator	63
Figure 41	: The buck/boost regulator topology	65
Figure 42	: The buck/boost regulator topology	66
Figure 43	: DC waveform for a buck/boost regulator	67
Figure 44	: AC waveforms for a buck/boost regulator	68
Figure 45	: Flyback regulator topology	70
Figure 46	: DC waveforms for a fly back regulator	71
Figure 47	: AC waveforms for a playback regulator	72
Figure 48	: The Half – forward regulator topology	74
Figure 49	: DC waveforms for a half – forward regulator	75
Figure 50	: AC waveform for a half – forward regulator	75
Figure 51	: The push – Pull Regulator Topology	77
Figure 52	: DC waveforms for a push – pull regulator	78
Figure 53	: AC Waveforms for a push-pull regulator	80
Figure 54	: The Full – Bridge Regulator Topology	82
Figure 55	: DC Waveforms for a full – bridge regulator	79
Figure 56	: AC waveforms for a full – bridge regulator	84
Figure 57	: The half – bridge regulator topology	86
Figure 58	: DC waveforms for a half-bridge regulator	87
Figure 59	: AC Waveforms for a half–bridge regulator	87
Figure 60	: A typical power supply	90
Figure 61	: Voltage regulator groupings	91
Figure 62	: Simple Zener Regulator	92

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 7 of 114
		Rev: 01
		Rev 01 – Jan 2016

Figure 63 : An op amp voltage regulator	93
Figure 64 : A Discrete voltage regulator	95
Figure 65 : A Voltage regulator with current limiting	96
Figure 66 : Configuration for an adjustable output three- terminal regulator	97
Figure 67 : D/A Controlled Voltage Regulator	98
Figure 68 : A three-terminal IC regulator with current boosting	99
Figure 69 : Current limiting schemes : (a) Simple current limiting, (b) foldback current limiting	100
Figure 70 : A 723 voltage regulator configured for foldback current limiting	101
Figure 71 : Contributors to thermal resistance	102
Figure 72 : Available regulator package styles	103

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 8 of 114
		Rev: 01
		Rev 01 – Jan 2016

INTRODUCTION

Scope

A power supply is an electronic device that supplies electric energy to an electrical load. The primary function of a power supply is to convert one form of electrical energy to another, as a result, power supplies are sometimes referred to as electric power converters. Some power supplies are discrete, stand alone devices, whereas others are built into larger devices along with their loads.

Depending on its design, a power supply may obtain energy from various types of energy sources, including electrical energy transmission systems, energy storage devices such as a batteries and fuel cells, electro mechanical systems such as generators and alternators, solar power converters, or another power supply.

This guideline provides an overview electrical power supply and regulation with the basic laws of electrical power supply, switching of power supply, and applications.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 9 of 114
		Rev: 01
		Rev 01 – Jan 2016

General Consideration

Power Supplies

Power supplies are used in many industrial and aerospace applications and in consumer products. Some of the requirements of power supplies are small size, light weight, low cost, and high power conversion efficiency. In addition to these, some power supplies require the following:

- electrical isolation between the source and load,
- low harmonic distortion for the input and output waveforms,
- and high power factor (PF) if the source is ac voltage.

Some special power supplies require controlled direction of power flow.

Basically two types of power supplies are required: direct current (DC) power supplies and alternating current (AC) power supplies. The input to these power supplies can be ac or dc.

DC Power Supplies

If an ac source is used electrical isolation can only be provided by bulky line frequency transformers. The ac source can be rectified with a diode rectifier to get an uncontrolled dc, and then a dc-to-dc converter can be used to get a controlled dc output. Electrical isolation between the input source and the output load can be provided in the dc – to – dc converter using a high-frequency (HF) transformer.

Such HF transformers have small size, light weight, and low cost compared to bulky line frequency transformers. Whether the input source is dc or ac, dc-to-dc converters form an important part of dc power supplies. DC power supplies can be broadly classified as linear and switching power supplies.

A linear power supply is the oldest and simplest type of power supply. The output voltage is regulated by dropping the extra input voltage across a series transistor (therefore, also referred to as a series regulator). They have very small output ripple, theoretically zero noise, large hold-up time (typically 1–2 ms), and fast response.

<p>KLM Technology Group</p> <p>Practical Engineering Guidelines for Processing Plant Solutions</p> <p>www.klmtechgroup.com</p>	<p>Kolmetz Handbook of Process Equipment Design</p> <p>ELECTRICAL POWER SUPPLY AND REGULATION</p> <p>(ENGINEERING DESIGN GUIDELINES)</p>	Page 10 of 114
		Rev: 01
		Rev 01 – Jan 2016

Linear power supplies have the following disadvantages: very low efficiency, electrical isolation can only be on 60-Hz ac side, larger volume and weight, and, in general, only a single output possible. However, they are still used in very small regulated power supplies and in some special applications. Three terminal linear regulator integrated circuits (ICs) are readily available, are easy to use, and have built-in load short-circuit protection.

Switching power supplies use power semiconductor switches in the on and off switching states, resulting in high efficiency, small size, and light weight. With the availability of fast switching devices, HF magnetics and capacitors, and high-speed control ICs, switching power supplies have become very popular. They can be further classified as pulse width-modulated (PWM) converters and resonant converters.

Pulse width – Modulated Converters

These converters employ square-wave pulse width modulation to achieve voltage regulation. The average output voltage is varied by varying the duty cycle of the power semiconductor switch. The voltage waveform across the switch and at the output are square wave in nature (refer to Figure 1 (b)) and they generally result in higher switching losses when the switching frequency is increased. Also, the switching stresses are high with the generation of large electromagnetic interference (EMI), which is difficult to filter. However, these converters are easy to control, well understood, and have wide load control range. The methods of control of PWM converters are discussed next.

The Methods of Control

The PWM converters operate with a fixed-frequency, variable duty cycle. Depending on the duty cycle, they can operate in either Continuous Current Mode (CCM) or discontinuous current mode (DCM). The three possible control methods [Severns and Bloom, 1988; Hnatek, 1981; Unitrode Corporation, 1984; Motorola, 1989; Philips Semiconductors, 1991] are briefly explained below.

1. Direct duty cycle control is the simplest control method. A fixed-frequency ramp is compared with the control voltage (Figure 1 (a)) to obtain a variable duty cycle base drive signal for the transistor. This is the simplest method of control. Disadvantages of this method are:

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 11 of 114
		Rev: 01
		Rev 01 – Jan 2016

- a) Provides no voltage feedforward to anticipate the effects of input voltage changes, slow response to sudden input changes, poor audio susceptibility, poor open-loop line regulation, requiring higher loop gain to achieve specifications.
 - b) Poor dynamic response.
2. Voltage feedforward control. In this case the ramp amplitude varies in direct proportion to the input voltage (Figure 1 (b)). The open-loop regulation is very good.
 3. Current mode control. In this method, a second inner control loop compares the peak inductor current with the control voltage which provides improved open-loop line regulation (Figure 1 (c)). All the problems of the direct duty cycle control method 1 above are corrected with this method. An additional advantage of this method is that the two-pole second-order filter is reduced to a single-pole (the filter capacitor) first-order filter, resulting in simpler compensation networks.

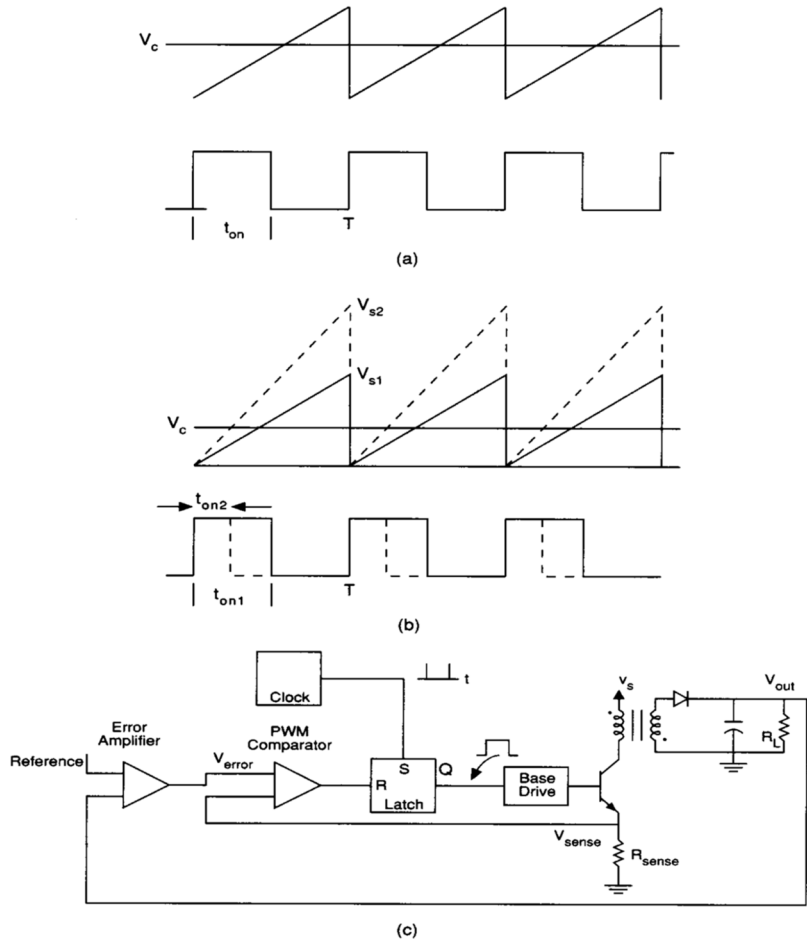


Figure 1: PWM Converter Methods: (a) direct duty cycle, (b) voltage feedforward control, (c) current mode control

PWM converters can be classified as single-ended and double-ended converters. These converters may or may not have a high-frequency transformer for isolation.

No isolated Single – Ended PWM Converters.

The basic nonisolated single-ended converters are: (a) buck (step-down), (b) boost (step-up), (c) buck-boost (step-up or step-down, also referred to as fly back), and (d) Cuk converters (Figure 2). The Cuk converter provides the advantage of non-pulsating input-output current ripple requiring smaller size external filters. Output voltage expression is

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 13 of 114
		Rev: 01
		Rev 01 – Jan 2016

the same as the buck-boost converter and can be less than or greater than the input voltage. There are many variations of the above basic nonisolated converters, and most of them use a high-frequency transformer for ohmic isolation between the input and the output.

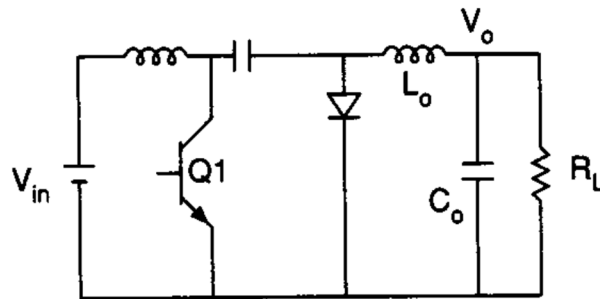


Figure 2: Nonisolated Cuk Converter

Isolated Single-Ended Topologies

1. The fly back converter (Figure 3) is an isolated version of the buck-boost converter. In this converter (Figure 3), when the transistor is on, energy is stored in the coupled inductor (not a transformer), and this energy is transferred to the load when the switch is off.

Some of the advantages of this converter are that the leakage inductance is in series with the output diode when current is delivered to the output, and, therefore, no filter inductor is required; cross regulation for multiple output converters is good; it is ideally suited for high-voltage output applications; and it has the lowest cost.

Some of the disadvantages are that large output filter capacitors are required to smooth the pulsating output current; inductor size is large since air gaps are to be provided; and due to stability reasons, fly back converters are usually operated in the DCM, which results in increased losses. To avoid the stability problem, fly back converters are operated with current mode control explained earlier. Fly back converters are used in the power range of 20 to 200 W.

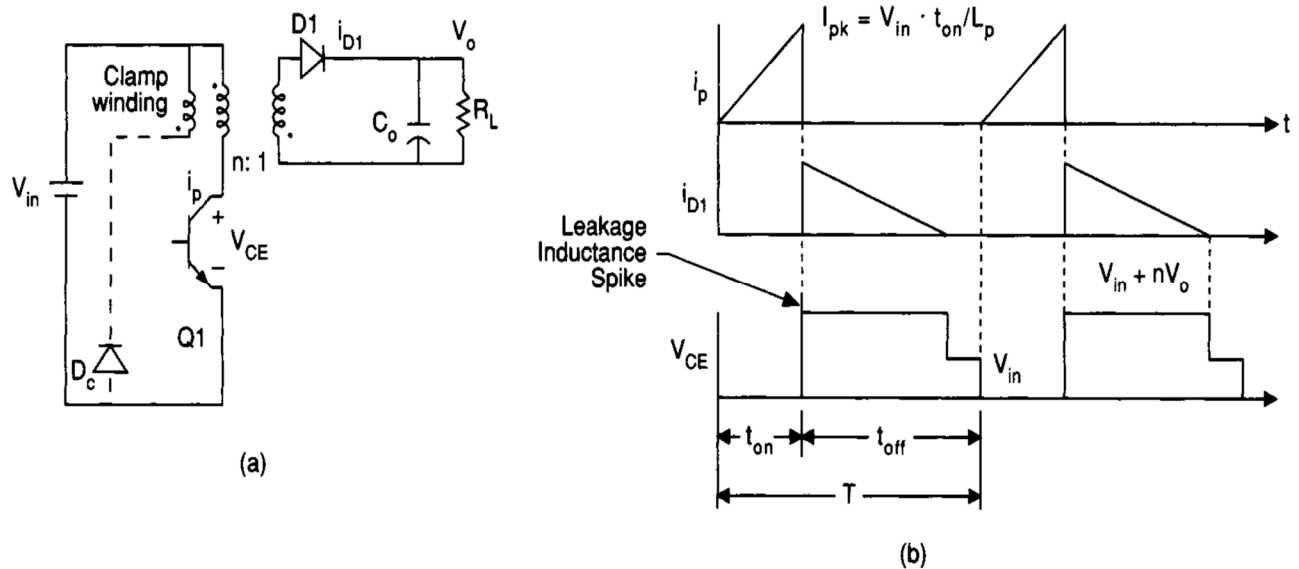


Figure 3:(a) Fly back converter. The clamp winding shown is optimal and is used to clamp the transistor voltage stress to $V_{in} + nV_o$ (b) Fly back converter waveforms without the clamp winding. The leakage inductance spikes vanish with the clamp winding.

2. The forward converter (Figure 4) is based on the buck converter. It is usually operated in the CCM to reduce the peak currents and does not have the stability problem of the fly back converter. The HF transformer transfers energy directly to the output with very small stored energy. The output capacitor size and peak current rating are smaller than they are for the fly back. Reset winding is required to remove the stored energy in the transformer. Maximum duty cycle is about 0.45 and limits the control range. This topology is used for power levels up to about 1 kW.

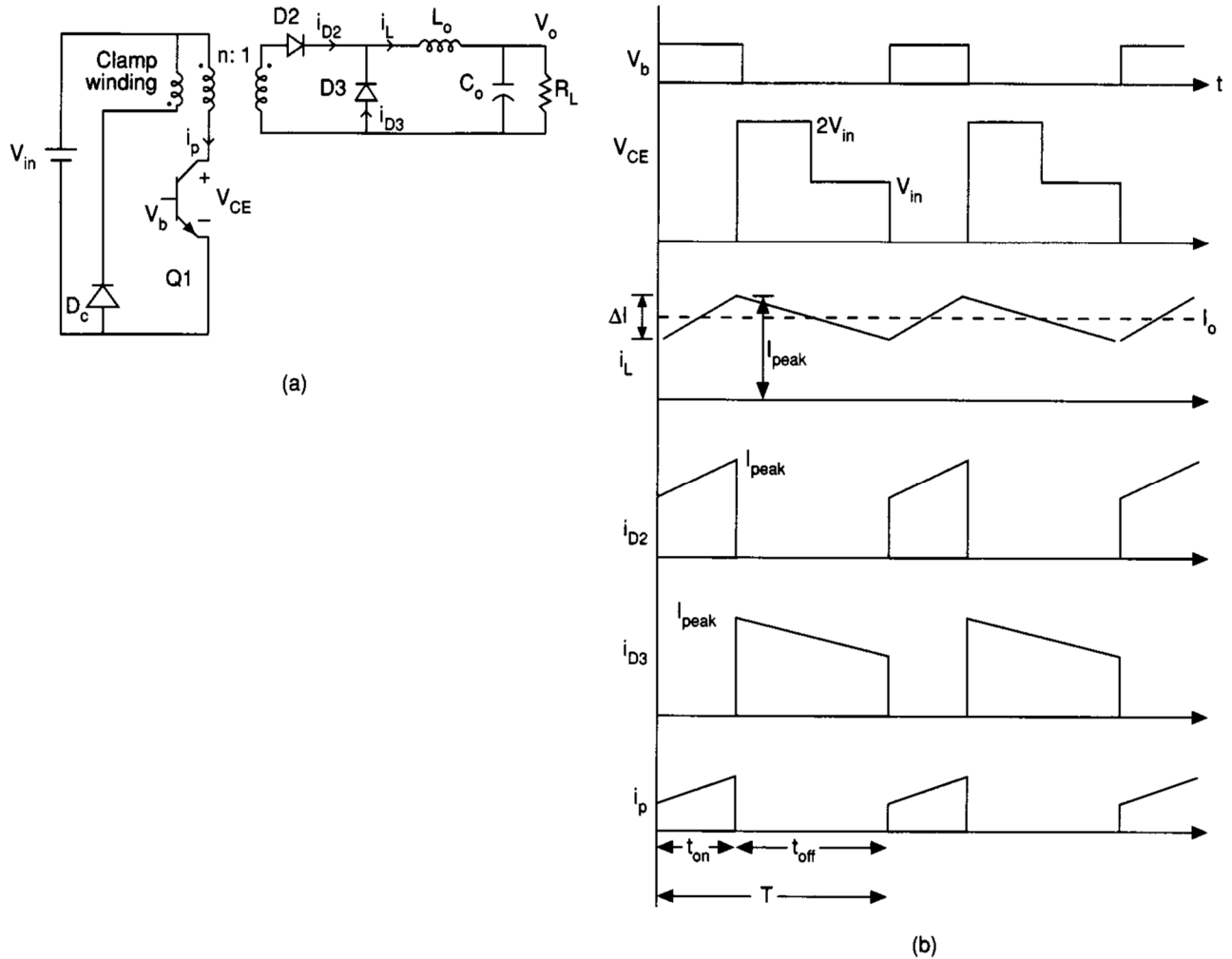


Figure 4:(a) Forward converter. The clamp winding shown is required for operation. (b) Forward converter waveforms.

3. The fly back and forward converters explained above require the rating of power transistors to be much higher than the supply voltage. The two-transistor fly back and forward converters shown in Figure 5 limit the voltage rating of transistors to the supply voltage.
4. The Sepic converter shown in Figure6 is another isolated single-ended PWM converter.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 16 of 114
		Rev: 01
		Rev 01 – Jan 2016

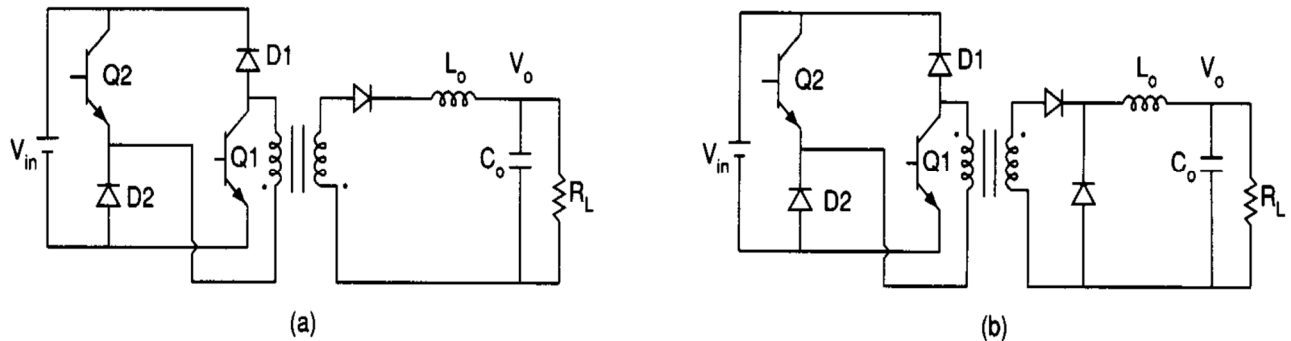


Figure 5:(a) Two – transistor single-ended fly back converter. (b) Two – transistor single – ended forward converter

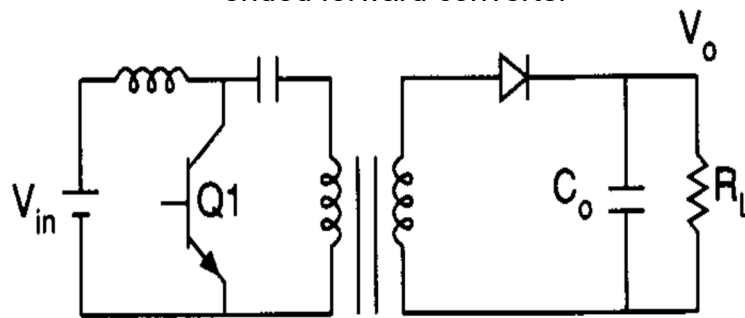


Figure 6: Sepic Converter

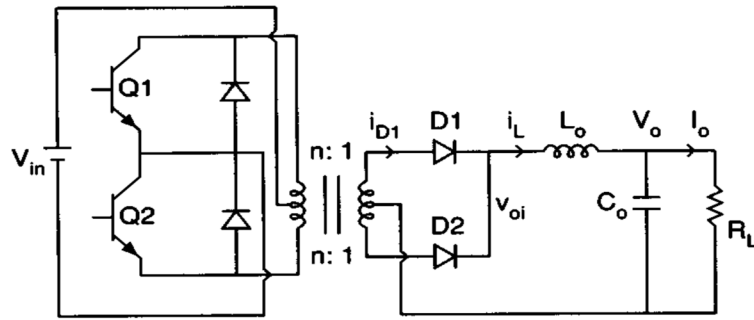
Double-Ended PWM Converters

Usually, for power levels above 300 W, double-ended converters are used. In double – ended converters, full-wave rectifiers are used and the output voltage ripple will have twice the switching frequency. Three important double-ended PWM converter configurations are push-pull (Figure 7), half-bridge (Figure 8), and full-bridge (Figure 9).

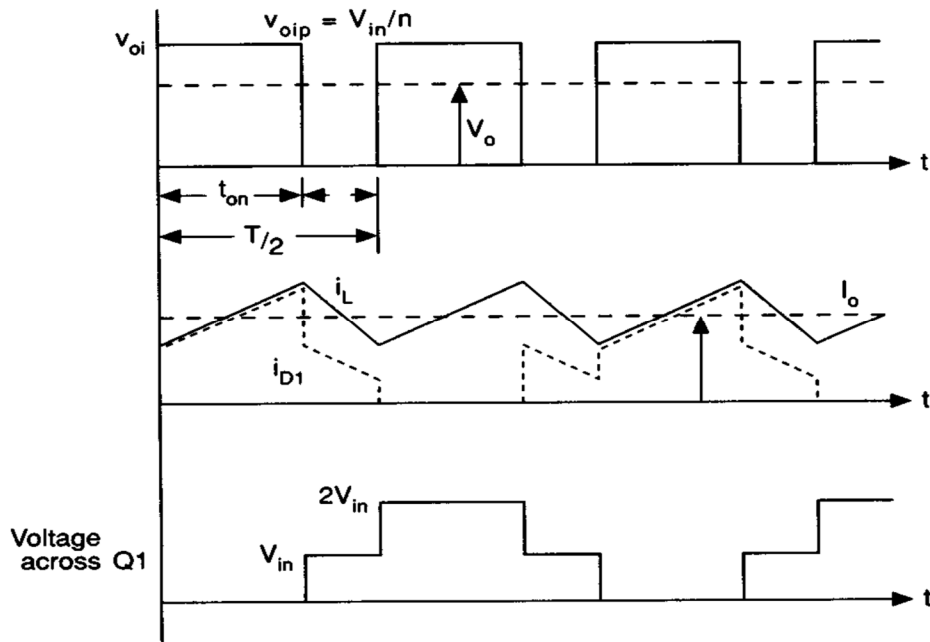
1. The push-pull converter. The duty ratio of each transistor in a push-pull converter (Figure 7) is less than 0.5. Some of the advantages are that the transformer flux swings fully, thereby the size of the transformer is much smaller (typically half the size) than single-ended converters, and output ripple is twice the switching frequency of transistors, allowing smaller filters. Some of the disadvantages of this configuration are that transistors must block twice the supply voltage, flux symmetry imbalance can cause transformer saturation and special control circuitry is required to avoid this problem, and use of center-tap transformer requires extra copper resulting in higher volt-ampere (VA) rating. Current mode

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 17 of 114
		Rev: 01
		Rev 01 – Jan 2016

control (for the primary current) can be used to overcome the flux imbalance. This configuration is used in 100- to 500-W output range.



(a)



(b)

Figure 7:(a) Push – pull converter and (b) its opening waveforms

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 18 of 114
		Rev: 01
		Rev 01 – Jan 2016

- The half-bridge. In the half-bridge configuration (Figure 8) center-tapped dc source is created by two smoothing capacitors (C_{in}), and this configuration utilizes the transformer core efficiently. The voltage across each transistor is equal to the supply voltage (half of push-pull) and, therefore, is suitable for high-voltage inputs. One salient feature of this configuration is that the input filter capacitors can be used to change between 110/220-V mains as selectable inputs to the supply. The disadvantage of this configuration is the requirement for large-size input filter capacitors. The half-bridge configuration is used for power levels of the order of 500 to 1000 W.

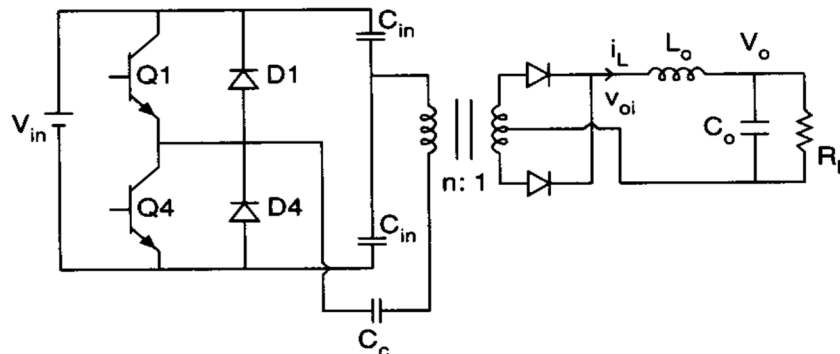


Figure 8:Half – bridge converter. Coupling capacitor C_c , is used to avoid transformer saturation.

- The full-bridge configuration (Figure 9) requires only one smoothing capacitor, and for the same transistor type as that of half-bridge, output power can be doubled. It is usually used for power levels above 1 kW, and the design is more costly due to increased number of components (uses four transistors compared to two in push-pull and half-bridge converters). One of the salient features of a full-bridge converter is that by using proper control technique it can be operated in zero-voltage switching (ZVS) mode. This type of operation results in negligible switching losses. However, at reduced load currents, the ZVS property is lost. Recently, there has been a lot of effort to overcome this problem.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 19 of 114
		Rev: 01
		Rev 01 – Jan 2016

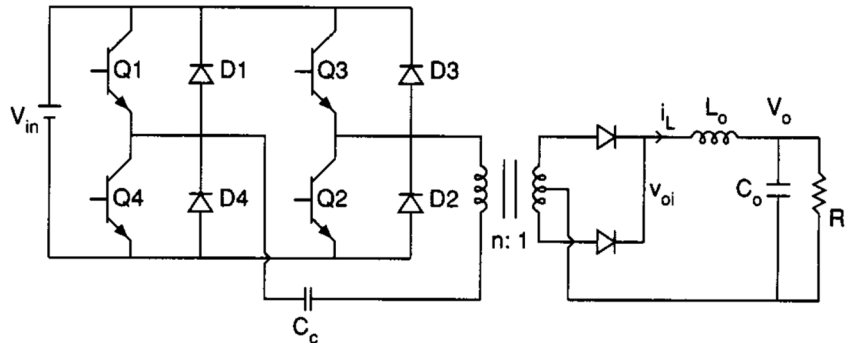


Figure9:Full – Bridge Converter

Resonant Power Supplies

Similar to the PWM converters, there are two types of resonant converters: single-ended and double-ended. Resonant converter configurations are obtained from the PWM converters explained earlier by adding LC (inductor-capacitor) resonating elements to obtain sinusoidally varying voltage and/or current waveforms. This approach reduces the switching losses and the switch stresses during switching instants, enabling the converter to operate at high switching frequencies, resulting in reduced size, weight, and cost. Some other advantages of resonant converters are that leakage inductances of HF transformers and the junction capacitances of semiconductors can be used profitably in the resonant circuit, and reduced EMI. The major disadvantage of resonant converters is increased peak current (or voltage) stress.

Single-Ended Resonant Converters

They are referred to as quasi-resonant converters (QRCs) since the voltage(or current) waveforms are quasi-sinusoidal in nature. The QRCs can operate with zero-current switching (ZCS) or ZVS or both. All the QRC configurations can be generated by replacing the conventional switches by the resonant switches shown in Figures 10 and 11. A number of configurations are realizable. Basic principles of ZCS and ZVS are explained briefly below.

1. Zero-current switching QRCs. Figure 12(a) shows an example of aZCS QR buck converter implemented using a ZC resonant switch. Depending on whether the resonant switch is half-wave type or full-wave type, the resonating current will be

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 20 of 114
		Rev: 01
		Rev 01 – Jan 2016

only half-wave sinusoidal (Figure 12 (b)) or a full sine-wave (Figure 12 (c)). The device currents are shaped sinusoidally, and, therefore, the switching losses are almost negligible with low turn-on and turn-off stresses. ZCS QRCscan operate at frequencies of the order of 2 MHz. The major problems with this type of converter are high peak currents through the switch and capacitive turn-on losses.

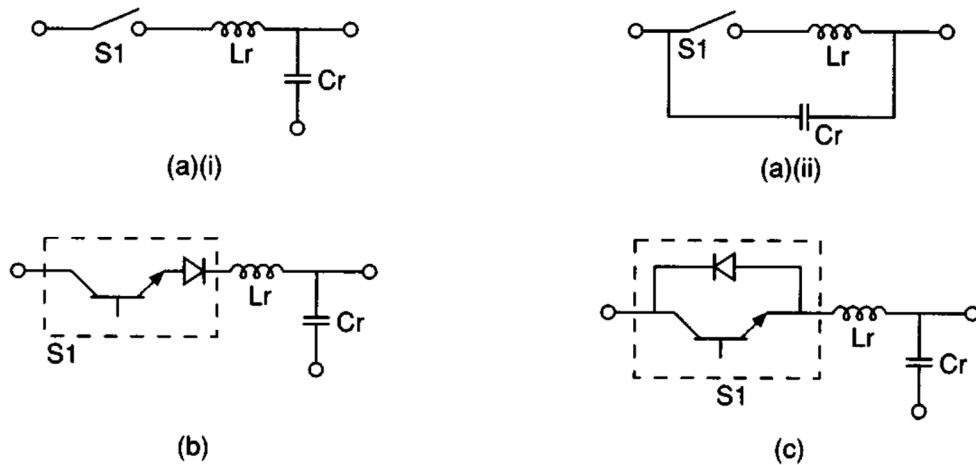


Figure 10:(a) Zero – current resonant switch: (i) L – type and (ii) M – Type. (b) Half wave configuration using L – Type ZC resonant switch. (c) Full – wave configuration using L – Type ZC resonant switch

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 21 of 114
		Rev: 01
		Rev 01 – Jan 2016

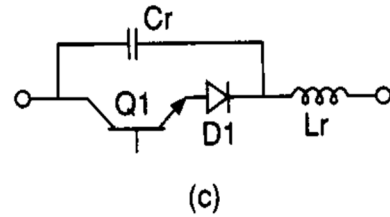
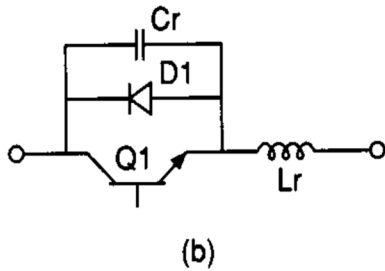
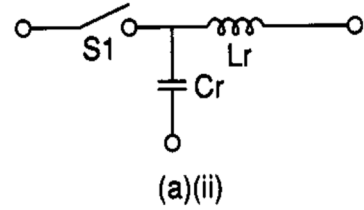
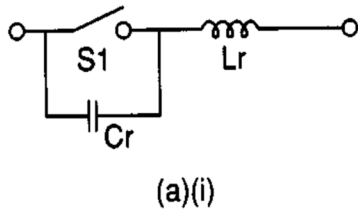


Figure 11: (a) Zero – voltage resonant switches. (b) Half – wave configuration using ZV resonant switch shown in Figure 10. (a)(i). (c) Full – wave configuration using ZV resonant switch shown in Figure (a)(i).

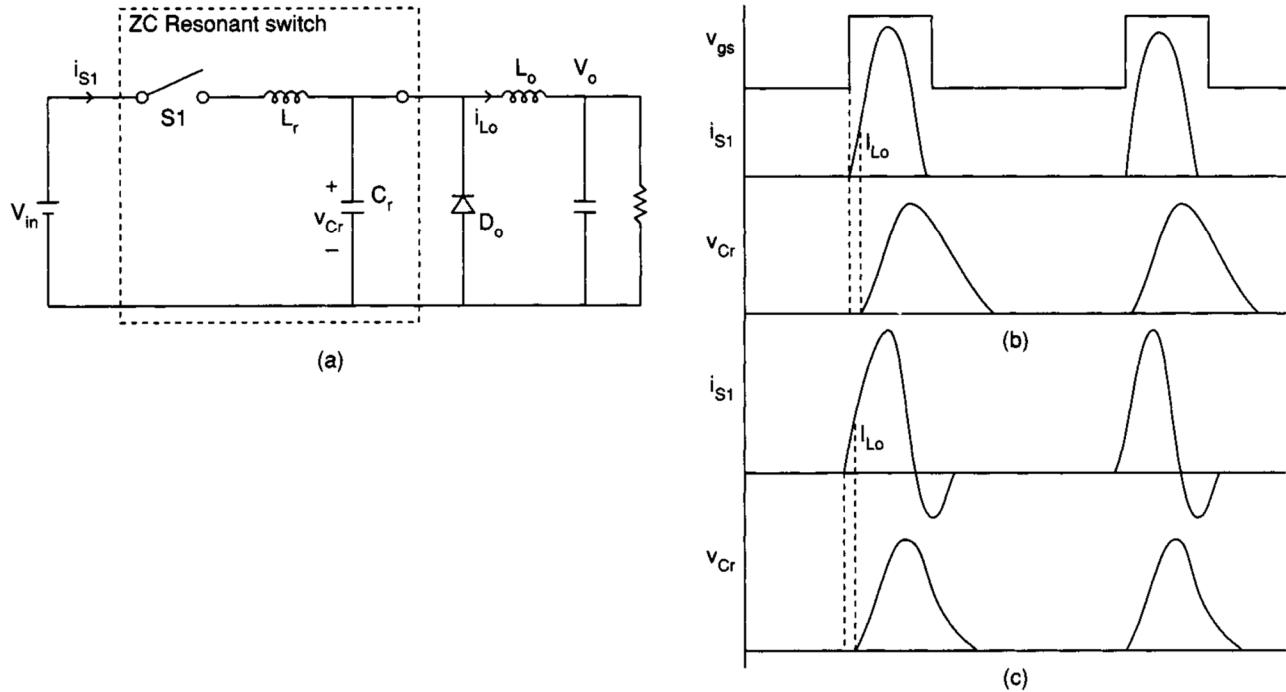


Figure 12: (a) Implementation of ZCS QR buck converter using L – Type resonant switch. (b) Operating waveforms for half – wave mode. (c) Operating waveforms for full – wave mode.

2. Zero-voltage switching QRCs. ZVS QRCs are duals of ZCS QRCs. The auxiliary LC elements are used to shape the switching device's voltage waveform at off time in order to create a zero-voltage condition for the device to turn on Figure 13(a) shows an example of ZVS QRboost converter implemented using a ZV resonant switch. The circuit can operate in the half-wave mode (Figure 13(b)) or in the full-wave mode (Figure 13(c)) depending on whether a half-wave or full-wave ZV resonant switch is used, and the name comes from the capacitor voltage waveform. The full-wavemode ZVS circuit suffers from capacitive turn-on losses. The ZVS QRCs suffer from increased voltage stress on the switch. However, they can be operated at much higher frequencies compared to ZCS QRCs.

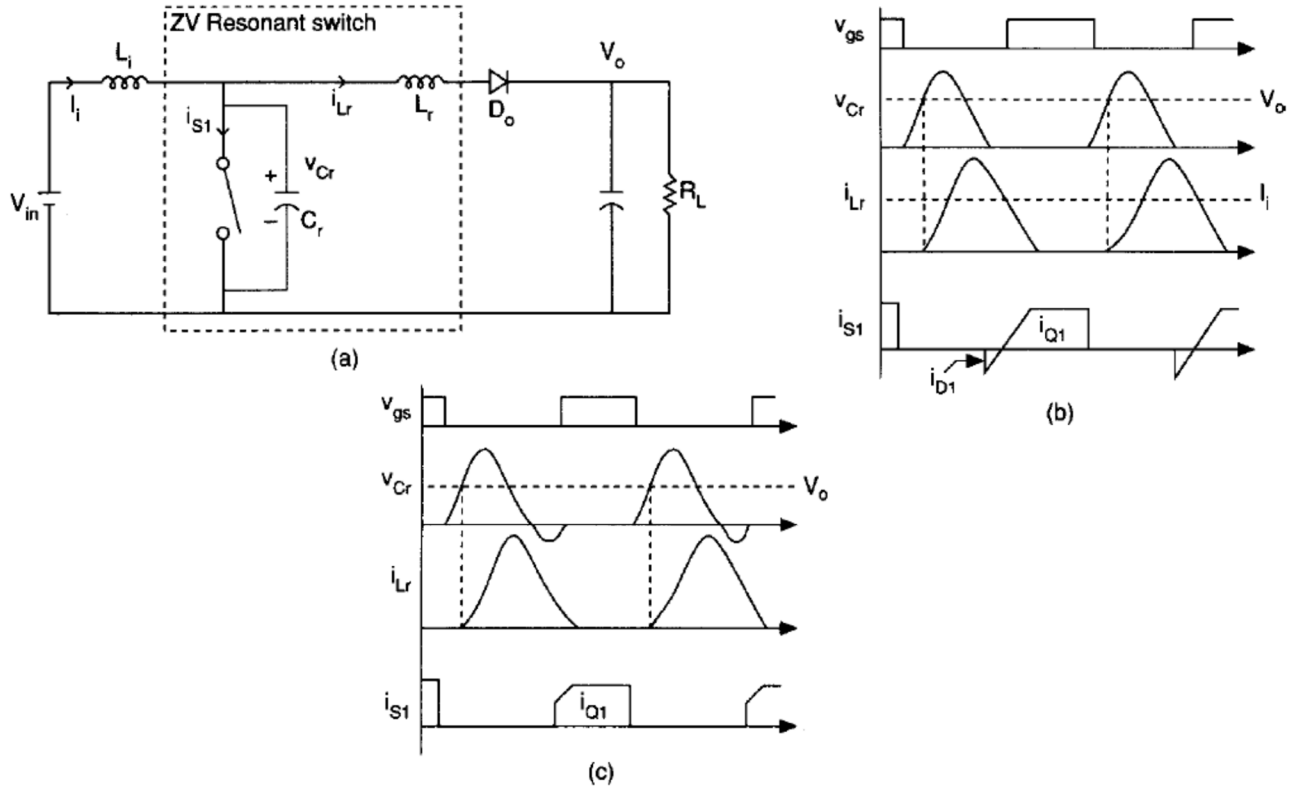


Figure 13: (a) Implementation of ZVS QR boost converter using resonant switch shown in Figure 12 (a) (i). (b) Opening waveforms for half-wave mode. (c) Operating waveforms for full-wave mode.

Double-Ended Resonant Converters

These converters use full-wave rectifiers at the output, and they are generally referred to as resonant converters. A number of resonant converter configurations are realizable by using different resonant tank circuits, and the three most popular configurations, namely, the series resonant converter (SRC), the parallel resonant converter (PRC), and the series-parallel resonant converter (SPRC) (also called LCC-type PRC), are shown in Figure 13. Series resonant converters (Figure 14. (a)) have high efficiency from full load to part load. Transformer saturation is avoided due to the series blocking resonating capacitor.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 24 of 114
		Rev: 01
		Rev 01 – Jan 2016

The major problems with the SRC are that it requires a very wide change in switching frequency to regulate the load voltage and the output filter capacitor must carry high ripple current (a major problem especially in low output voltage, high output current applications).

Parallel resonant converters (Figure 14(b)) are suitable for low output voltage, high output current applications due to the use of filter inductance at the output with low ripple current requirements for the filter capacitor. The major disadvantage of the PRC is that the device currents do not decrease with the load current, resulting in reduced efficiency at reduced load currents.

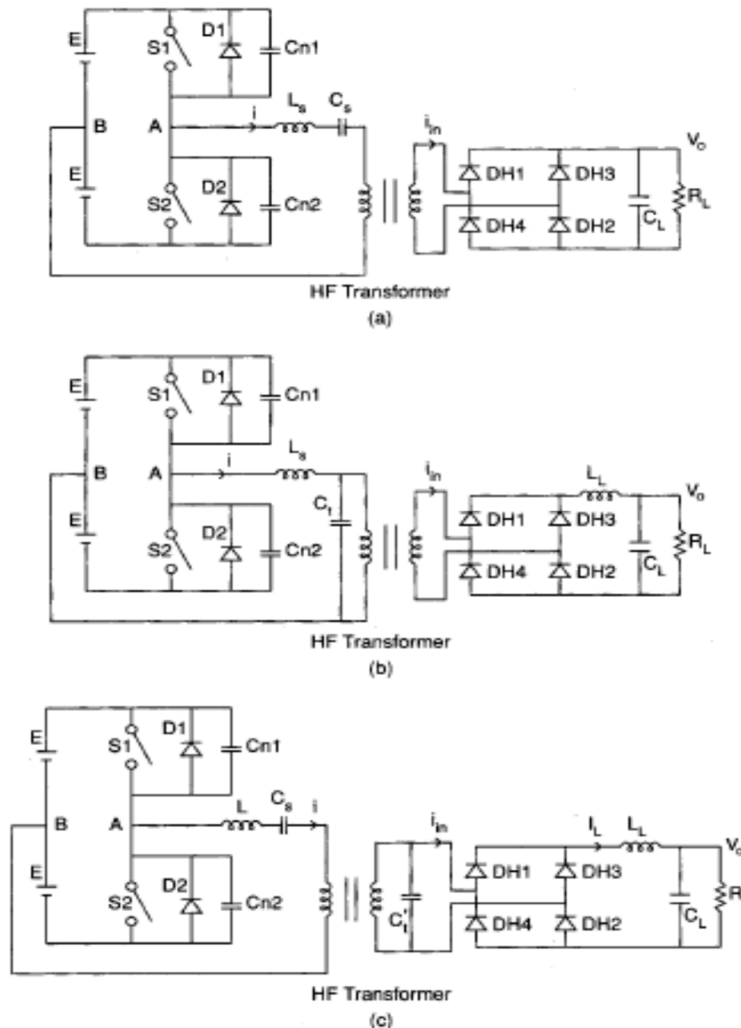


Figure 14: High-frequency resonant converter (half-bridge version) configurations suitable for operation above resonance. C_{n1} and C_{n2} are the snubber capacitors. (a) Series resonant converter. Leakage inductances of the HF transformer can be part of resonant inductance. (b) Parallel resonant converter. (c) Series-parallel (or LCC-type) resonant converter with capacitor C_t placed on the secondary side of the HF transformer.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 26 of 114
		Rev: 01
		Rev 01 – Jan 2016

Definitions

- Current** : The density of the atoms in copper wire is such that the valence orbits of the individual atoms overlap.
- Current Limiting** : A technique used to provide short-circuit protection. Typically, current sensing resistor is used to turn a transistor on and off that in turn is used to provide negative feedback to hold the output current at a high but safe value.
- Dropout Voltage** : The input – output voltage differential at which the circuit ceases to regulate against further reductions in input voltage.
- Diode** : A semiconductor device made up of a P and n type semiconductor type.
- Filter Circuit** : The circuit used to filter out AC ripple from DC.
- Fly back Regulator** : The technique by which the regulated load power is transferred during the off time of the switching device.
- Fold back Current Limiting** : A more sophisticated type of short – circuit protection in which the output current is cut dramatically back, not just held constant.
- Forward Regulator** : The technique by which the regulated load power is transferred during the on time of the switching device.
- Inductance** : The property which opposes any change in the existing current. Inductance is present only when the current is changing.
- Line Regulation** : The percent change of output voltage for a change in input supply voltage.
- Linear Regulator** : Voltage regulator using a transistor operating in the linear region.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 27 of 114
		Rev: 01
		Rev 01 – Jan 2016

- Load Regulation : The percent change of output voltage for a change in output current.
- Low dropout voltage : Refers to a class of voltage regulators designed to operate at especially low input-output voltage differentials.
- Magneto motive Force (mmf) : The product of the current and the number of turns in the transformer.
- Rectifier : A device that converts AC signals to DC.
- Regulator : An electronic device that attempts to keep the output signal constant in spite of changes in the other system characteristics.
- Resistor : Made of materials that conduct electricity, but offer opposition to current flow.
- Ripple : The fluctuation on the DC input signal to the voltage regulator, caused by the charging and discharging of the capacitor input filter.
- Ripple Rejection : A measure of how well the regulator attenuates the input ripple, usually specified in decibels.
- Ripple Voltage : The AC voltage associated with the DC in a rectifier circuit.
- Switching Regulator : A voltage that operates by using a saturating switching transistor to chop an unregulated DC voltage. This chopped voltage is then filtered. The duty cycle of the switching transistor is varied to provide regulation of the output voltage.
- Topology : The overall design technique, or layout, by which an electronic device, such as a switching power supply regulator, operates.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 28 of 114
		Rev: 01
		Rev 01 – Jan 2016

- Transformers : A device used to step up or step down the AC voltage and to isolate mains supply from the rectifier circuit.
- Voltage : The basic unit of measure for potential difference is the volt (symbol V), and because the volt unit is used, potential difference is called voltage.
- Voltage regulator : That part of a power supply that accepts a filtered DC voltage and reduces, if not eliminates, the ripple, providing a continuous, smooth DC signal.

KLM Technology Group Practical Engineering Guidelines for Processing Plant Solutions www.klmtechgroup.com	Kolmetz Handbook of Process Equipment Design ELECTRICAL POWER SUPPLY AND REGULATION (ENGINEERING DESIGN GUIDELINES)	Page 29 of 114
		Rev: 01
		Rev 01 – Jan 2016

Nomenclature

A	: Cross-sectional Area
A_L	: Inductance index in milli
D	: Diodes
i	: Current
I_{load}	: Load DC Current
L	: winding inductance
N	: Number of turns in the coil
R	: Resistance
R_p	: Primary windings resistance
R_s	: Secondary windings resistance
R_{se}	: Equivalent resistance in the secondary circuit
ρ	: Permeance of the core material
t	: Time
v	: Voltage
r_D	: diode resistance
V_{Do}	: diode forward voltage
V_{DC}	: DC output voltage from the filter
V_i	: the input voltage
V_{load}	: load DC Voltage
X_m	: Magnetizing resistance
X_p	: Primary windings leakage resistance
X_s	: Secondary winding leakage resistance
X_{se}	: Equivalent leakage resistance in the secondary circuit
W	: Energy
Z	: Impedance

Greek Letters

α_{Ti}	: Temperature coefficient
μ	: Permeability
ϕ	: Magnetic Flux
θ	: Angle